

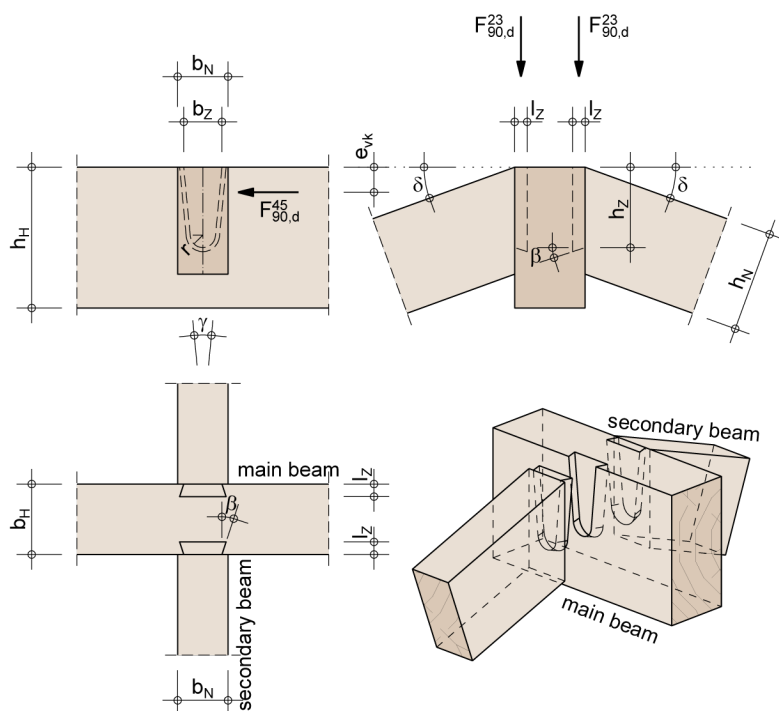
Verification Dovetail-Connection

according to building approval Z-9.1-649 (validity 18 June 2018 - 5 October 2022)

Connection & Geometry

double-sided connection

material:	laminated timber
solidity:	GL24c according to DIN EN 14080:2013-09
width secondary beam b_N :	120 mm
height secondary beam h_N :	240 mm
width main beam b_H :	160 mm
height main beam h_H :	320 mm
inclination δ :	30 °
milling angle β :	10 °
pin cone angle γ :	4 °
length pin l_Z :	28 mm
width pin b_Z :	110 mm
height pin h_Z :	218 mm
pin hole radius r :	47.7 mm
dimensional tolerances:	+/- 0.2 mm



Loads

Load $F_{23,90,d}$:	13.00 kN
Load $F_{45,90,d}$:	0.00 kN
e_{vk} :	0 mm
Service class:	NKL1 - heated interiors
KLED:	medium
modification factor k_{mod} :	0.8

Verification:

$0.98 \leq 1.00$

Verification fulfilled

Construction tip

Building approval Z-9.1-649 must be observed.

Stress resistance in insertion direction

$$k_n: \quad 6.50$$

$$\alpha = \cos(\delta) * \frac{h_Z - r}{h_N} = \cos(30) * \frac{218 - 47.7}{240} = 0.61$$

$$k_v = \min \left\{ \begin{array}{l} 1 \\ \frac{k_n}{\sqrt{h_N} * (\sqrt{\alpha} * (1 - \alpha) + 0.4 * \frac{l_Z}{h_N} * \sqrt{\frac{1}{\alpha} - \alpha^2})} \end{array} \right.$$

$$= \min \left\{ \begin{array}{l} 1 \\ \frac{6.50}{\sqrt{240} * (\sqrt{0.61} * (1 - 0.61) + 0.4 * \frac{28}{240} * \sqrt{\frac{1}{0.61} - 0.61^2})} \end{array} \right.$$

$$= \min \left\{ \begin{array}{l} 1 \\ 0.78 \end{array} \right.$$

$$k_{ab}: \quad 0.80$$

$$f_{t,90,d}: \quad 0.308 \text{ N/mm}^2 \quad (\text{with } f_{t,90,k} = 0.5 \text{ N/mm}^2 \text{ according to approval})$$

$$f_{v,d}: \quad 1.538 \text{ N/mm}^2 \quad (\text{with } f_{v,k} = 2.5 \text{ N/mm}^2 \text{ according to approval})$$

$$F_{90,Rd}^{23} = \min \left\{ \begin{array}{l} k_{ab} * \frac{h_Z}{h_Z - r} * \left(6.5 + \frac{18 * (h_H - h_Z + r)^2}{h_H^2} \right) * (t_{ef} * h_H)^{0.8} * f_{t,90,d} \\ \frac{k_v * b_N * (h_Z - r)}{1.5} * f_{v,d} \end{array} \right.$$

$$= \min \left\{ \begin{array}{l} 0.80 * \frac{218}{218 - 47.7} * \left(6.5 + \frac{18 * (320 - 218 + 47.7)^2}{320^2} \right) * (100 * 320)^{0.8} * 0.308 \\ \frac{0.78 * 120 * (218 - 47.7)}{1.5} * 1.538 \end{array} \right.$$

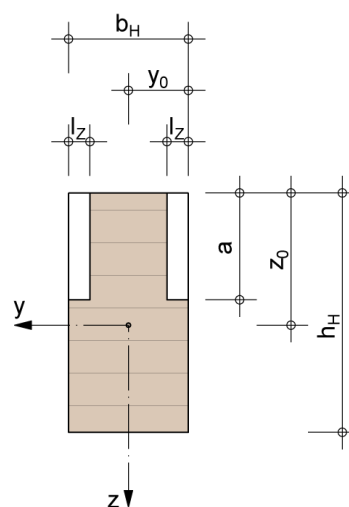
$$= \min \left\{ \begin{array}{l} 13.22 \\ 16.28 \end{array} \right.$$

$$\text{stress resistance } F_{90,Rd}^{23}: \quad 13.22 \text{ kN}$$

Verification in insertion direction:	$\frac{F_{90,d}^{23}}{F_{90,Rd}^{23}} = \frac{13.00}{13.22} =$	$0.98 \leq 1.00$
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Cross-sectional weakening

width main beam b_H :	160 mm
height main beam h_H :	320 mm
height a :	222.9 mm
length pin l_Z :	28 mm
position of centre y_0 :	80.0 mm
position of centre z_0 :	175.6 mm
moment of inertia I_y :	34631 cm ⁴



moment of inertia of the unattenuated main beam:

$$I_{y,H} = \frac{b_H * h_H^3}{12} = \frac{160 * 320^3}{12} * 10^{-4} = 43691 \text{ cm}^4$$

required cross-sectional height with the same moment of inertia I_y related to the unattenuated cross-sectional of the main beam:

width beam b_H :	160 mm
height beam h_{erf} :	346 mm
height a :	222.9 mm
length pin l_Z :	28 mm
position of centre y_0 :	80.0 mm
position of centre z_0 :	190.9 mm
moment of inertia I_y :	43955 cm ⁴

